

Surface integral equations for dielectrics

- We can now derive a set of coupled surface integral equations for the tangential components of the electric and magnetic fields (they are continuous across interface)

$$0 = \mathbf{E}_i(\mathbf{r}') - j\omega\mu_0 \oint_S \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS$$

$\mathbf{r}' \rightarrow S$ from V_d

$$+ \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS$$

$$0 = -j\omega\mu_0 \oint_S \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS$$

$\mathbf{r}' \rightarrow S$ from V_0

$$+ \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS$$

Surface integral equations for dielectrics

- ❑ There seems to be a discrepancy here. There are 4 unknown fields (tangential components of E and H) but six equations!
- ❑ But actually two of those are redundant. To see this take the right hand side of the 2nd equation.
- ❑ For $r' \in V_0$, this is the field of equivalent surface electric and magnetic currents on S , generated in V_0 if V_0 is filled with the same material as the object. But if the tangential component of this electric field is zero on S (as $r' \rightarrow S$) then all the components of the field (including normal component) will be zero in V_0

Surface integral equations for dielectrics

- Hence, we only need to consider the tangential part:

$$0 = -j\omega\mu_0\hat{\mathbf{n}}' \times \oint_S \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS \\ + \hat{\mathbf{n}}' \times \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS$$

- A similar argument applies to the 1st equation so that

$$-\hat{\mathbf{n}}' \times \mathbf{E}_i(\mathbf{r}') = -j\omega\mu_0\hat{\mathbf{n}}' \times \oint_S \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS \\ + \hat{\mathbf{n}}' \times \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS$$

Surface integral equations for dielectrics

- The same can be done using the magnetic field formulation

$$\begin{aligned} -\hat{\mathbf{n}}' \times \mathbf{H}_i(\mathbf{r}') &= \hat{\mathbf{n}}' \times \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS \\ &\quad + j\omega\epsilon_0 \hat{\mathbf{n}}' \times \oint_S \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS \end{aligned} \quad \mathbf{r}' \rightarrow S \text{ from } V_d$$

$$\begin{aligned} 0 &= \hat{\mathbf{n}}' \times \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS \\ &\quad + j\omega\epsilon_d \hat{\mathbf{n}}' \times \oint_S \bar{\bar{\mathbf{G}}}_d(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS \end{aligned} \quad \mathbf{r}' \rightarrow S \text{ from } V_0$$

Surface integral equations for dielectrics

- Let us be more specific. Note that in terms of the scalar Green's function

$$\bar{\bar{\mathbf{G}}}(\mathbf{r}', \mathbf{r}) = G(\mathbf{r}', \mathbf{r}) \bar{\bar{\mathbf{I}}} - \frac{1}{k^2} \nabla' \nabla G(\mathbf{r}', \mathbf{r})$$

$$\begin{aligned} \left[\nabla' \times \bar{\bar{\mathbf{G}}}(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] &= \nabla' G(\mathbf{r}', \mathbf{r}) \times [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] \\ &= \nabla' \times [G(\mathbf{r}', \mathbf{r}) \hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] \end{aligned}$$

$$\begin{aligned} \bar{\bar{\mathbf{G}}}(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] &= G(\mathbf{r}', \mathbf{r}) [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] \\ &\quad - \frac{1}{k^2} \nabla' \left\{ \nabla G(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] \right\} \end{aligned}$$

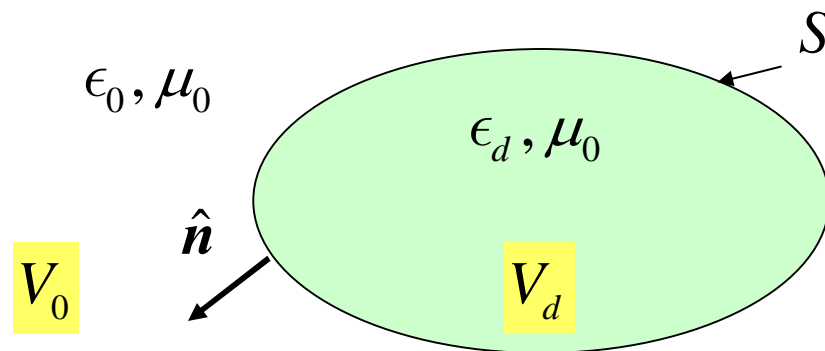
Surface integral equations for dielectrics

- Once these equations are solved, the surface fields can be used to evaluate the scattered field everywhere outside the object by using the Huygens principle:

$$\begin{aligned}
 \mathbf{E}(\mathbf{r}') = \mathbf{E}_i(\mathbf{r}') &- j\omega\mu_0 \oint_S \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \cdot [\hat{\mathbf{n}} \times \mathbf{H}(\mathbf{r})] dS \\
 &+ \oint_S \left[\nabla' \times \bar{\bar{\mathbf{G}}}_0(\mathbf{r}', \mathbf{r}) \right] \cdot [\hat{\mathbf{n}} \times \mathbf{E}(\mathbf{r})] dS
 \end{aligned}$$

Scattered field

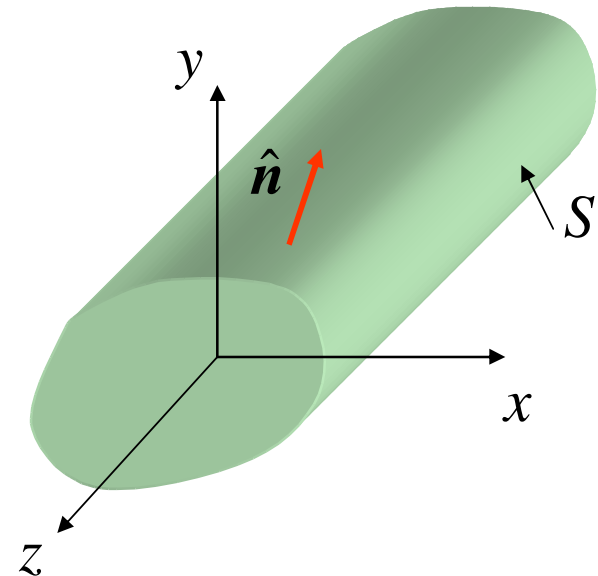
$$\mathbf{r}' \in V_0$$



2D surface integral equations

- ❑ Let us give an example: we consider a cylindrical object extended in the z -direction and restrict ourselves to solutions *uniform* in the z -direction (2D problem)
- ❑ We can again distinguish the TE and TM solutions:
- ❑ TE: H has only a z -component and E lies on the x - y plane
- ❑ TM: E has only a z -component and H lies on the x - y plane

$$\boldsymbol{\rho} = (x, y)$$



2D surface integral equations (TM)

- For the 2D TM problem the electric field equations can be written as

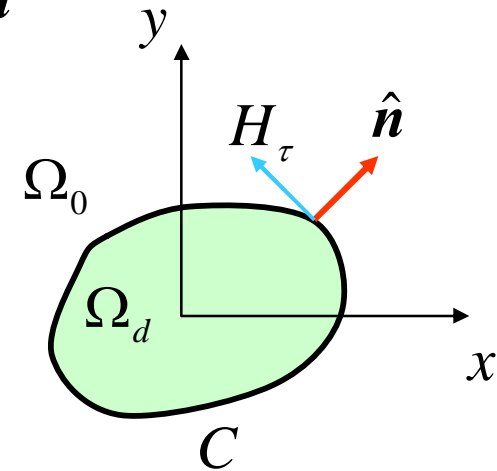
$$-E_{i,z}(\boldsymbol{\rho}') = -j\omega\mu_0 \oint_C G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_\tau(\boldsymbol{\rho}) dl - \oint_C \partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_z(\boldsymbol{\rho}) dl$$

$$\partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \equiv -\nabla G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} = \nabla' G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} \quad \boldsymbol{\rho}' \rightarrow C \text{ from } \Omega_d$$

$$= -\lim_{\zeta \rightarrow 0} \nabla G_0^{(2D)}(\boldsymbol{\rho}' - \zeta \hat{\mathbf{n}}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}}$$

- Here we have introduced the magnetic field tangential to the boundary curve as

$$H_\tau(\boldsymbol{\rho}) = [\hat{\mathbf{n}} \times \mathbf{H}(\boldsymbol{\rho})] \cdot \hat{\mathbf{z}}$$



2D surface integral equations (TM)

- The other equation

$$0 = -j\omega\mu_0 \oint_C G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_\tau(\boldsymbol{\rho}) dl + \oint_C \partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_z(\boldsymbol{\rho}) dl$$

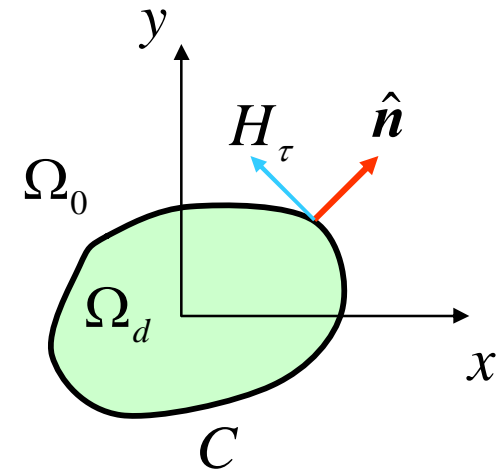
$$\partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \equiv \nabla G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} = -\nabla' G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} \quad \boldsymbol{\rho}' \rightarrow C \text{ from } \Omega_0$$

$$= \lim_{\zeta \rightarrow 0} \nabla G_d^{(2D)}(\boldsymbol{\rho}' + \zeta \hat{\mathbf{n}}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}}$$

- In all these equations

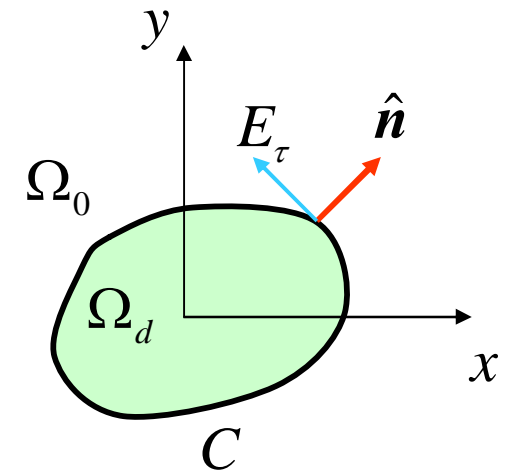
$$G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \frac{1}{4j} H_0^{(2)}(k_0 |\boldsymbol{\rho}' - \boldsymbol{\rho}|)$$

$$G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \frac{1}{4j} H_0^{(2)}(k_d |\boldsymbol{\rho}' - \boldsymbol{\rho}|)$$



2D surface integral equations (TE)

- Now, for the TE case we use the magnetic field formulation. We now have a magnetic field along z and an electric field on the x-y plane (uniformity is again assumed along z)



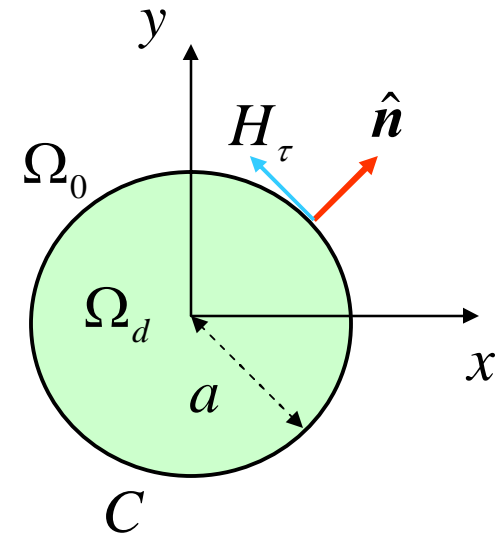
$$-H_{i,z}(\boldsymbol{\rho}') = j\omega\epsilon_0 \oint_C G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_\tau(\boldsymbol{\rho}) dl - \oint_C \partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_z(\boldsymbol{\rho}) dl$$

$$0 = j\omega\epsilon_d \oint_C G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_\tau(\boldsymbol{\rho}) dl + \oint_C \partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_z(\boldsymbol{\rho}) dl$$

- Now we can define surface *impedance* functions and an equivalent surface magnetic current for the incident field

2D surface integral equations (TE)

- Let us treat a circular dielectric cylinder. Of course we can exactly solve it using the usual cylindrical vector functions. But here we apply the surface integral technique.
- For the TM case:



$$-E_{i,z}(\boldsymbol{\rho}') = -j\omega\mu_0 \oint_C G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_\tau(\boldsymbol{\rho}) dl - \oint_C \partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_z(\boldsymbol{\rho}) dl$$

$$0 = -j\omega\mu_0 \oint_C G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) H_\tau(\boldsymbol{\rho}) dl + \oint_C \partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) E_z(\boldsymbol{\rho}) dl$$

Dielectric cylinder

- Let us see what the Green's functions are on the surface

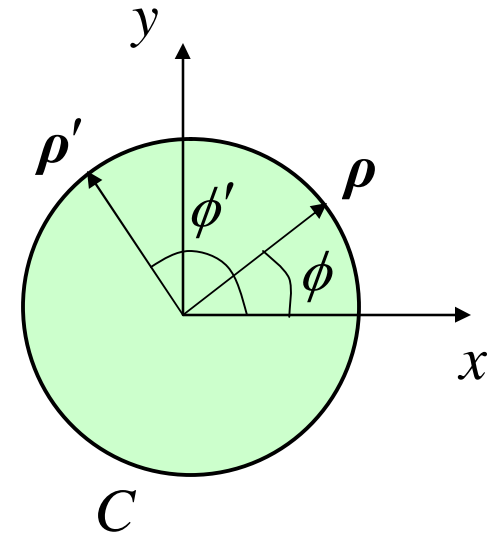
$$G^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \frac{1}{4j} H_0^{(2)}(k|\boldsymbol{\rho}' - \boldsymbol{\rho}|)$$

- We use the addition theorem

$$H_0^{(2)}\left(\sqrt{u^2 + v^2 - 2uv \cos \beta}\right) = \sum_{m=-\infty}^{\infty} H_m^{(2)}(u) J_m(v) \exp(-jm\beta) \quad u \geq v$$

$$G^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \frac{1}{4j} \sum_{m=-\infty}^{\infty} H_m^{(2)}(ka) J_m(ka) \exp[-jm(\phi' - \phi)]$$

$$k = k_0, k_d$$



Dielectric cylinder

- Now for the other functions:

$$\partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = -\nabla G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} = -\frac{\partial G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho})}{\partial \rho} \quad \boldsymbol{\rho}' \rightarrow C \text{ from } \Omega_d$$

$$\partial_n^- G_0^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = -\frac{k_0}{4j} \sum_{m=-\infty}^{\infty} H_m^{(2)'}(k_0 a) J_m(k_0 a) \exp[-jm(\phi' - \phi)]$$

- Moreover:

$$\partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \nabla G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) \cdot \hat{\mathbf{n}} = \frac{\partial G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho})}{\partial \rho} \quad \boldsymbol{\rho}' \rightarrow C \text{ from } \Omega_0$$

$$\partial_n^+ G_d^{(2D)}(\boldsymbol{\rho}', \boldsymbol{\rho}) = \frac{k_d}{4j} \sum_{m=-\infty}^{\infty} H_m^{(2)}(k_d a) J'_m(k_d a) \exp[-jm(\phi' - \phi)]$$

Dielectric cylinder

Resulting equations

$$\begin{aligned} -4j\mathbf{e}_{i,m} &= -j\omega\mu_0 2\pi a H_m^{(2)}(k_0 a) J_m(k_0 a) \mathbf{h}_m \\ &\quad + 2\pi k_0 a H_m^{(2)'}(k_0 a) J_m(k_0 a) \mathbf{e}_m \end{aligned}$$

$$\begin{aligned} 0 &= -j\omega\mu_0 2\pi a H_m^{(2)}(k_d a) J_m(k_d a) \mathbf{h}_m + \\ &\quad 2\pi k_d a H_m^{(2)'}(k_d a) J_m(k_d a) \mathbf{e}_m \end{aligned}$$

$$\begin{Bmatrix} \mathbf{h}_m \\ \mathbf{e}_m \\ \mathbf{e}_{i,m} \end{Bmatrix} = \frac{1}{2\pi} \int_0^{2\pi} \begin{Bmatrix} H_\tau(\phi') \\ E_z(\phi') \\ E_{i,z}(\phi') \end{Bmatrix} \exp(jm\phi') d\phi'$$

Dielectric cylinder

$$\rightarrow \mathbf{h}_m = \frac{1}{j\omega\mu_0 a} \frac{(k_d a) J'_m(k_d a)}{J_m(k_d a)} \mathbf{e}_m$$

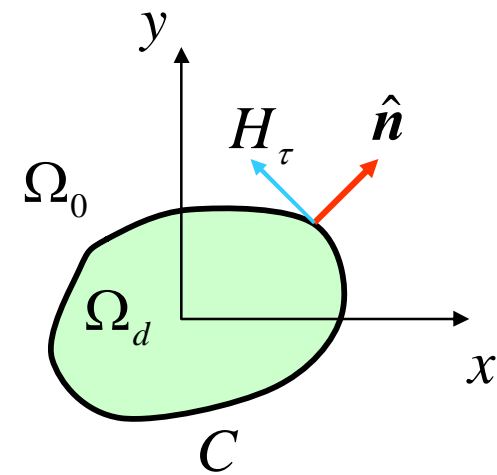
$$-\frac{2j}{\pi} \mathbf{e}_{i,m} = H_m^{(2)}(k_0 a) J_m(k_0 a)$$

$$\left[\frac{(k_0 a) H_m^{(2)'}(k_0 a)}{H_m^{(2)}(k_0 a)} - \frac{(k_d a) J'_m(k_d a)}{J_m(k_d a)} \right] \mathbf{e}_m$$

- The solved coefficients can then be used to evaluate the surface fields and, next, the overall field outside the object by using the Huygens principle

Surface integral equations for dielectrics

- In general, however, the solution to the line 2D or surface (3D) boundary integral equations should be obtained numerically, e.g. by using the method of moments



This document was created with Win2PDF available at <http://www.win2pdf.com>.
The unregistered version of Win2PDF is for evaluation or non-commercial use only.
This page will not be added after purchasing Win2PDF.